

Sensitivity and Uncertainty Methods for Fuel Cycle Analysis

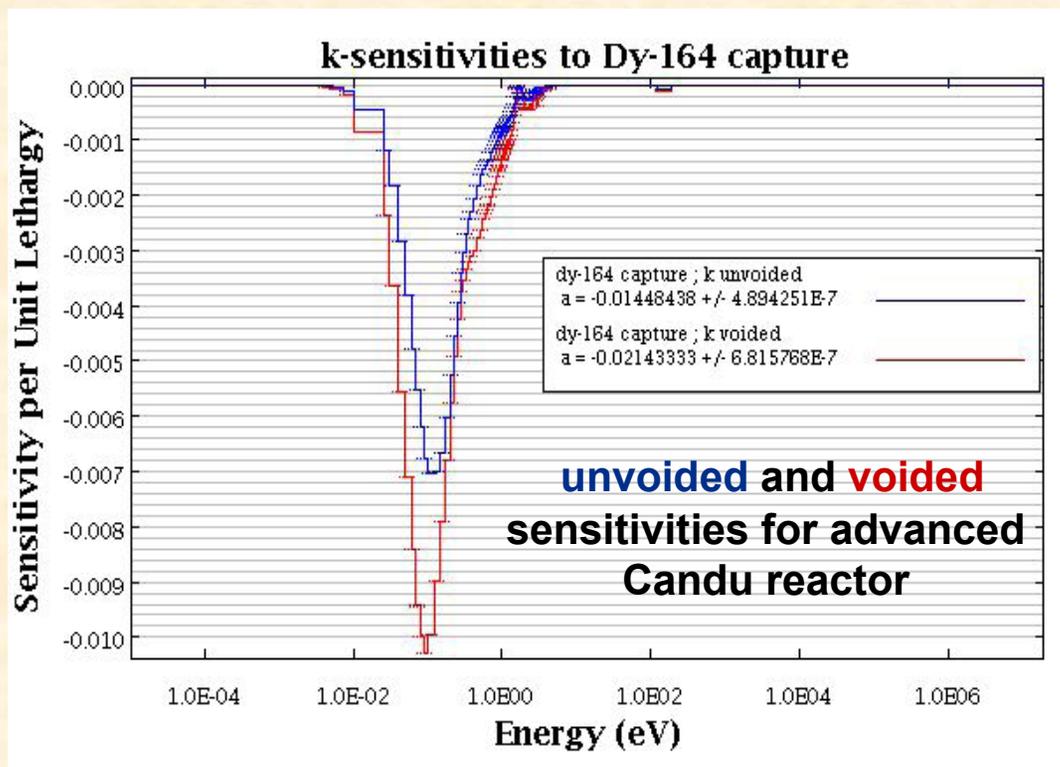
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Sensitivity Coefficients Reveal the Relation Between Nuclear Data and Applications

$$\left(\frac{\delta k}{k} \right) = S_{k,\sigma} \left(\frac{\delta \sigma}{\sigma} \right)$$



S/U Methods Can Be Used to Assess Impact of Data on Design of AFC Facilities

- **REACTOR CORE**
 - Core performance and safety parameters
 - Fuel cycle

- **CRITICALITY SAFETY AND SHIELDING**
 - Fuel fabrication
 - Reprocessing/recycling facilities
 - Transportation of spent fuel
 - Rad-waste disposition facilities

Applications of S/U Methods

- Determine sensitivity of calculated results to nuclear data used in transport calculations
- Determine uncertainty in calculations due to data uncertainties
- Identify relative contributions of nuclear data to uncertainty
- Perform similarity analysis of application vs. experiments to select or design integral benchmark experiments
- Adjust differential and integral data to obtain greater consistency
- Determine computational bias and uncertainty in response, based on benchmark experiment analysis

In 1970-80's S/U Methods Were Developed for (mainly) LMFBR Analysis

Limitations of Earlier S/U Methods

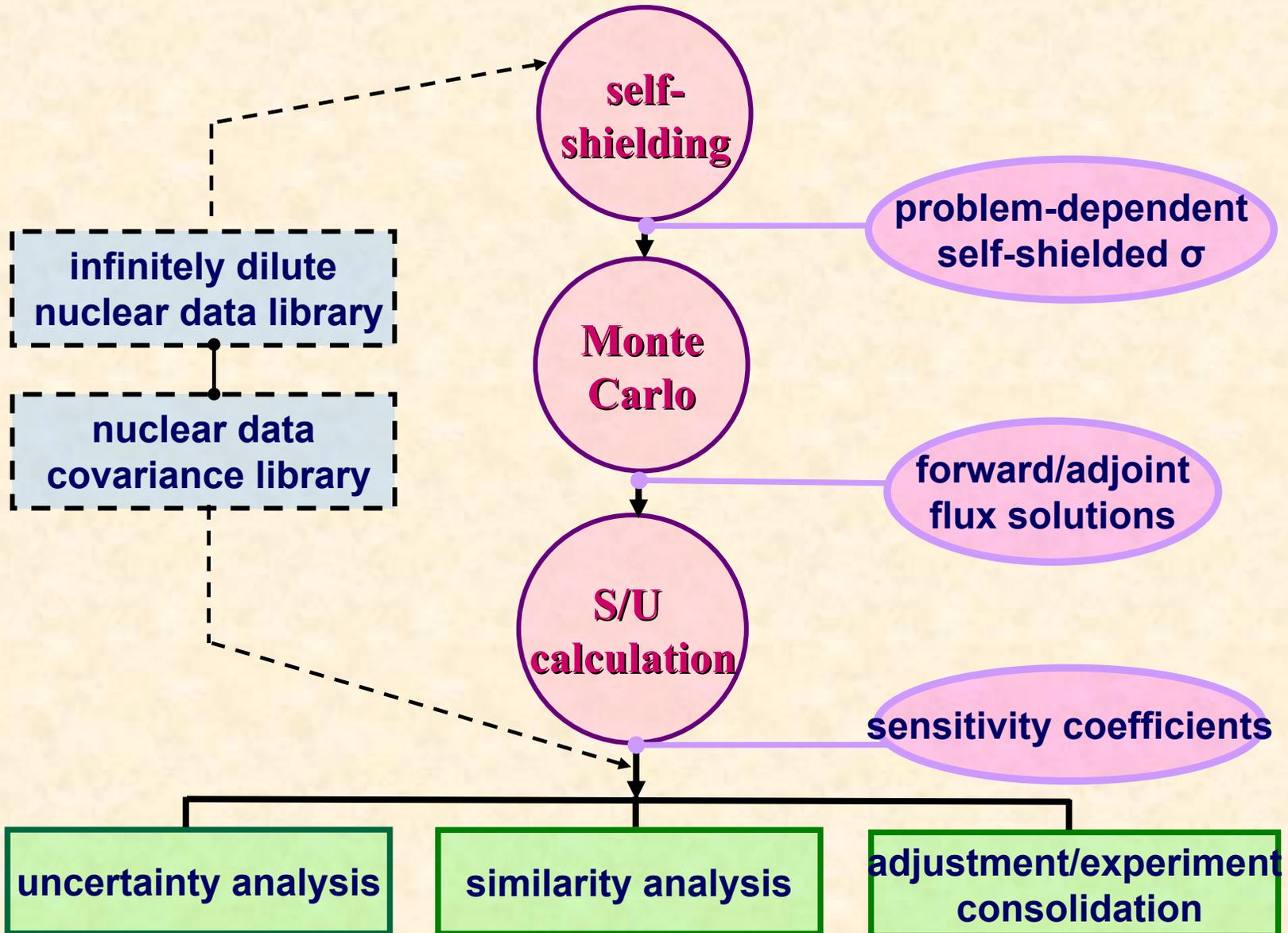
- Limited to homogenized transport models, often based on 1D/2D discrete ordinates or 3D diffusion theory
- Could not address thermal systems with significant resonance self-shielding sensitivities
- Lack of cross section covariance data
- Difficult to use— required setting up multiple calculations:
 - radiation transport
 - sensitivity coefficients
 - uncertainty analysis

TSUNAMI

The Next Generation of S/U Methods at ORNL

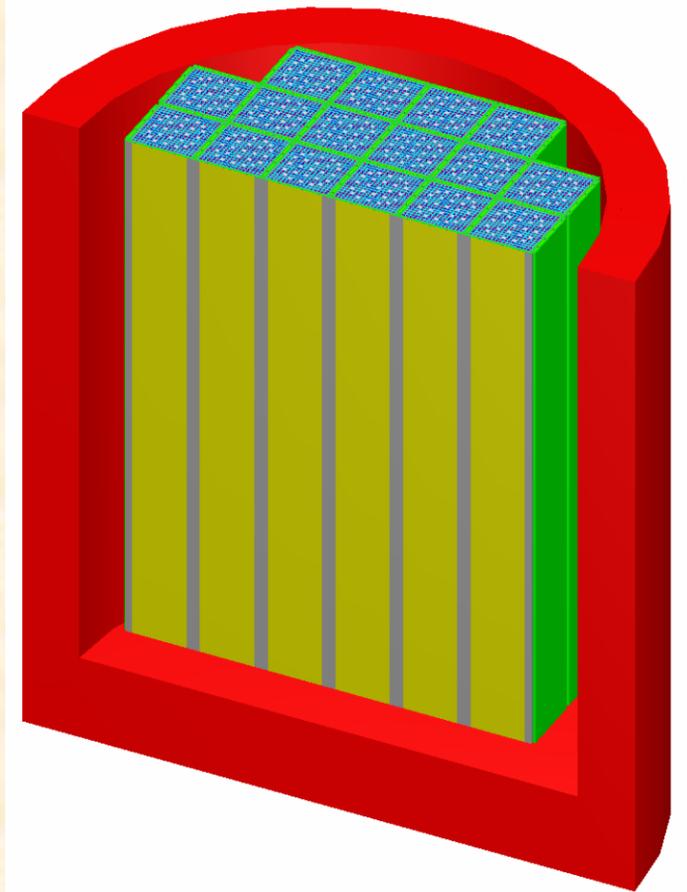
- Entire computation sequence is automated
- Sensitivity calculation based on 3D Monte Carlo or 1D SN
- Sensitivity coefficients include effects of perturbations in resonance self-shielding
- A more complete covariance library is available, based on integral approximation
- GUI's are available for displaying S/U information
- Modules available for similarity analysis and data adjustment

TSUNAMI-3D Computation Sequence

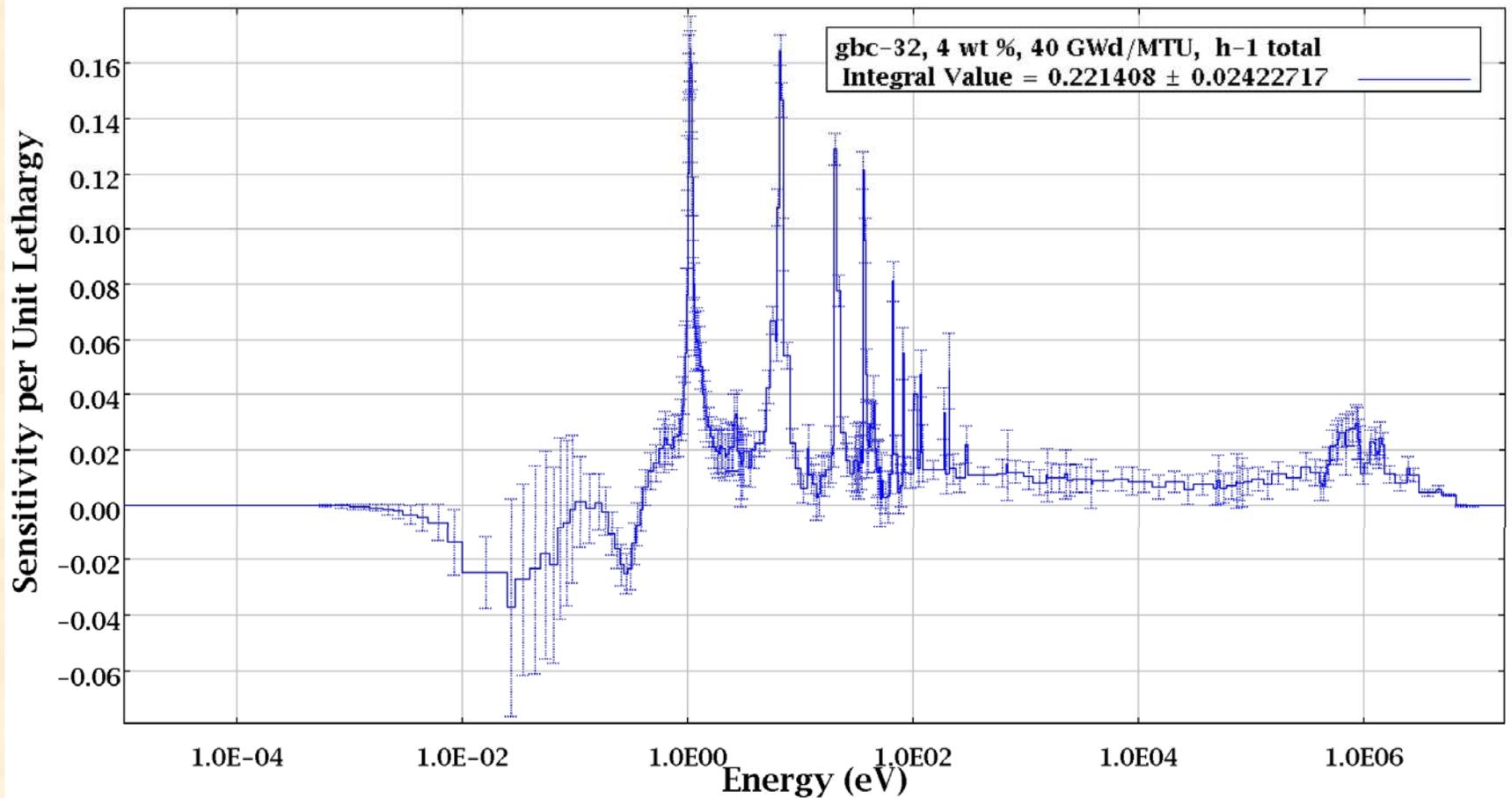


Burnup Credit Cask Model for S/U Analysis with Monte Carlo

- 32 PWR fuel assemblies
- 4 wt% Westinghouse 17x17 assemblies
- 18 axial burnup zones
- Burned to 40 GWd/MTU; Cooled for 5 years
- BORAL™ plates around each assembly
- 23.76 cm (9.353") cell pitch
- Cask filled with water
- Referred to as the GBC-32 (for details see NUREG/CR-6747)



TSUNAMI-3D Calculation for H Total Sensitivity in Shipping Cask



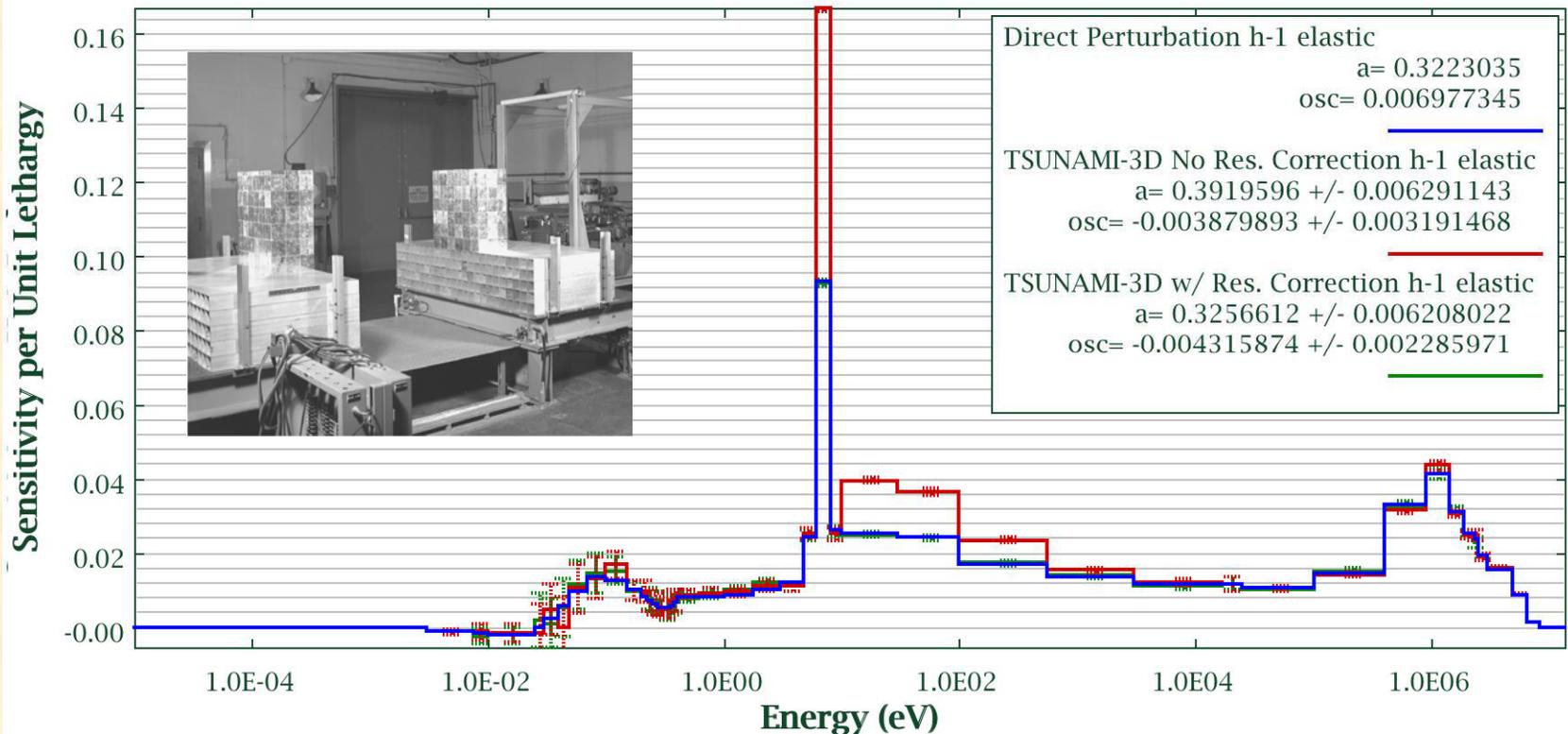
Complete Sensitivity Coefficient Includes *Implicit* and *Explicit* Effects

- **“Explicit Effect”** =
sensitivity to changes in multigroup cross sections appearing transport equation
- **“Implicit Effect”** =
sensitivity to cross section perturbations caused by changes in self-shielding

Example:

A perturbation in $\sigma^{(H)}$ changes self-shielded $\sigma^{(U238)}$;
→ implicit perturbation in $\sigma^{(U238)}$ changes k_{eff}

Sensitivity Coefficient for H Elastic in Thermal Critical Experiment



Approximate Covariance Library for TSUNAMI Applications

- Covariance data for >50 nuclides were taken from ENDF/B-VI, JENDL-3.3, or JEFF-3.1 if available
- Covariance data for >250 nuclides are approximated by **integral measurement uncertainties**
 - σ_s (moderators) ~ potential cross section uncertainty
 - $\sigma_c, \sigma_{f,u}$ [$E < 0.5$ eV] ~ thermal data uncertainty
 - σ_c, σ_f [$0.5 < E < 5E3$ eV] ~ resonance integral uncertainty

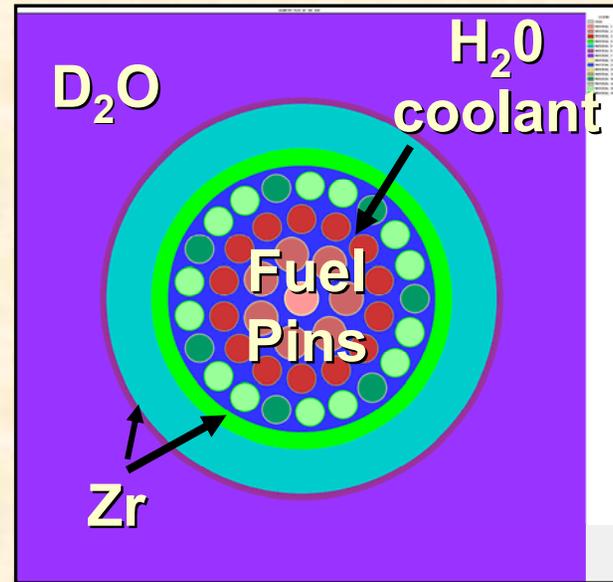
NO UNCERTAINTIES INCLUDED FOR $E > 5E3$ eV

Differential versus Integral Data and Uncertainties

Resonance Integrals

Nuclide	ENDF/B VI	Integral experiment	difference (%)	integral uncertainty (%)
Cd-113	3.92E+2	3.90E+2	0.5	10.3
Xe-135	7.65E+6	7.60E+3	0.7	6.6
Sm-149	4.02E+4	4.01E+4	0.2	5.9
Np-237	6.60E+2	6.40E+2	3.0	7.8

Example Uncertainty Analysis: coolant void reactivity in advanced Candu reactor



Response	Relative St. Dev. (%)
Eigenvalue, <i>unvoided</i>	0.80
Eigenvalue, <i>voided</i>	0.84
coolant void reactivity	49.8

Example Uncertainty Analysis: Space-Reactor Shielding

Shield Design	Response ; <i>Uncertainty %</i>	Major Contributors to Uncertainty
<hr/> SS316 <hr/> B4C <hr/> Be + B4C	$\phi > 1\text{MeV}$ 6.01%	o-16 n,n'
		h-1 elastic
		o-16 elastic
		o-16 n,alpha
		li-6 elastic
<hr/> SS316 <hr/> Water+LiOH	Si γ-Kerma 1.34%	fe-56 n,gamma
		cr-53 n,gamma
		ni-58 n,gamma
		mn-55 n,gamma
<hr/> SS316 <hr/>	Peak Heating 0.28%	b-10 n,alpha
fe-56 elastic		

Similarity Analysis

Similarity parameter c_k is system correlation coefficient between a design system and a critical experiment

$$c_k(\mathbf{A}, \mathbf{E}) = \frac{\text{Cov}[\mathbf{A}, \mathbf{E}]}{[\text{std}(\mathbf{A})] [\text{std}(\mathbf{E})]} = \frac{\mathbf{S}_A \text{Cov}[\boldsymbol{\sigma}, \boldsymbol{\sigma}] \mathbf{S}_E^\dagger}{[\text{std}(\mathbf{A})] [\text{std}(\mathbf{E})]}$$

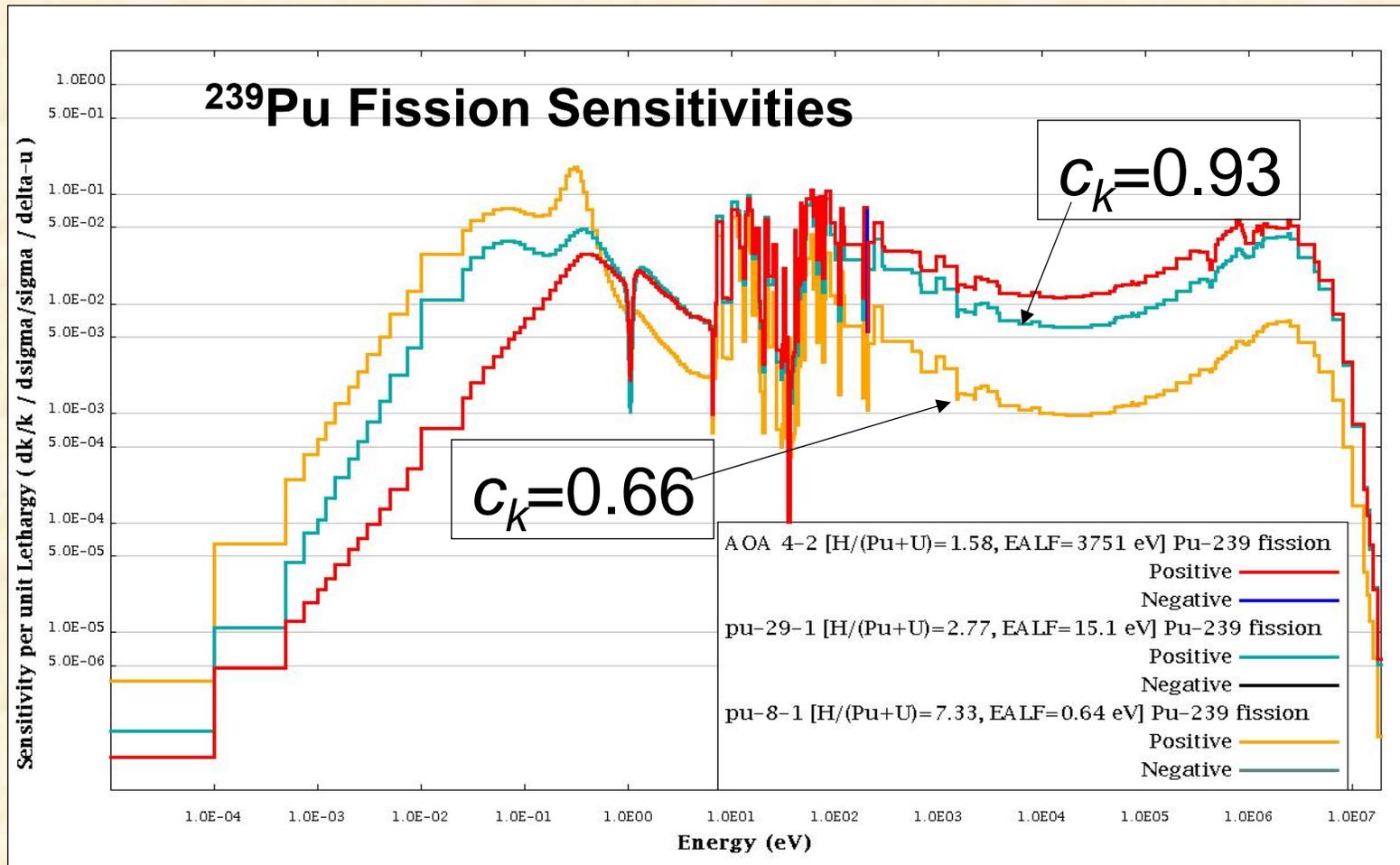
Premise: Computational bias is caused largely by uncertainties in cross section data

- Systems with similarly high sensitivities to same cross-section uncertainty data will have similar computational biases

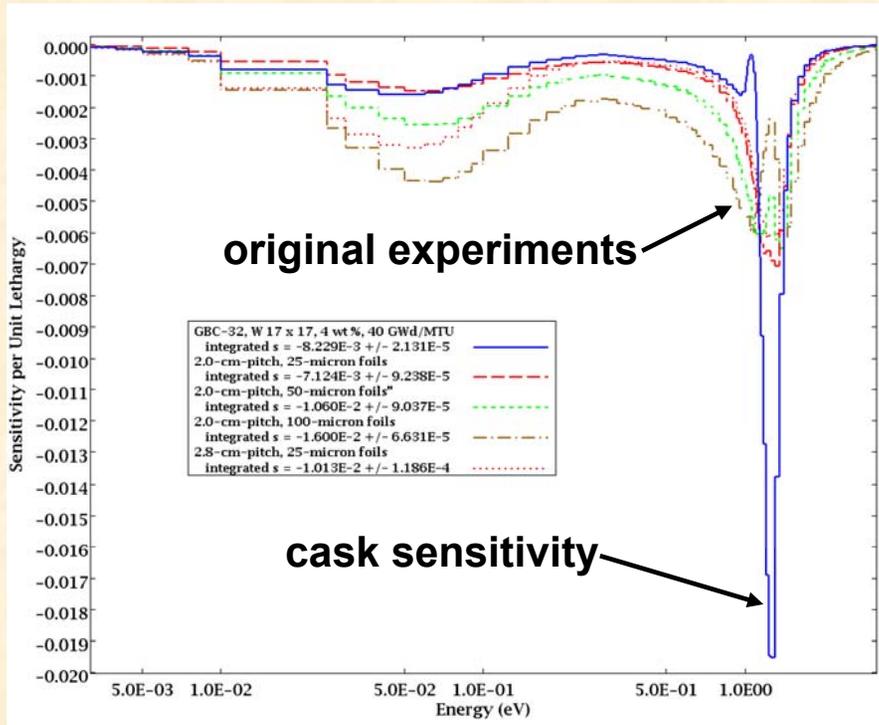
● **Normalized:** such that

- $c_k = 1.0$ indicates systems are fully correlated ;
- $c_k = 0.0$ indicates systems are completely uncorrelated
- $c_k = -1.0$ indicates systems are fully anti-uncorrelated

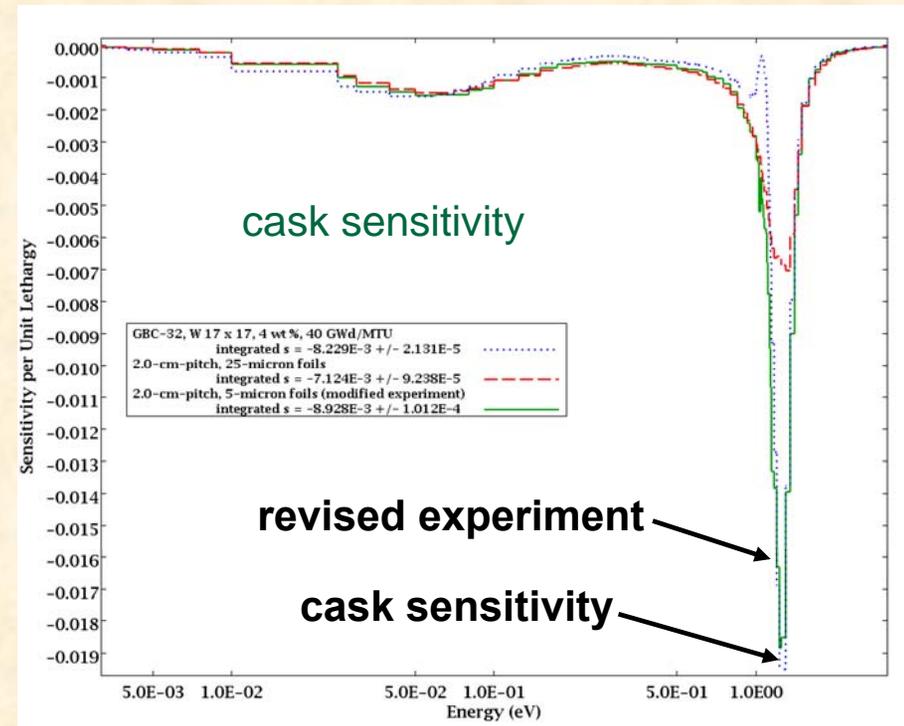
EXAMPLE SIMILARITY ANALYSIS: Selection of Benchmark Experiments for Criticality Safety Validation



EXAMPLE SIMILARITY ANALYSIS: Integral experiment design for shipping cask



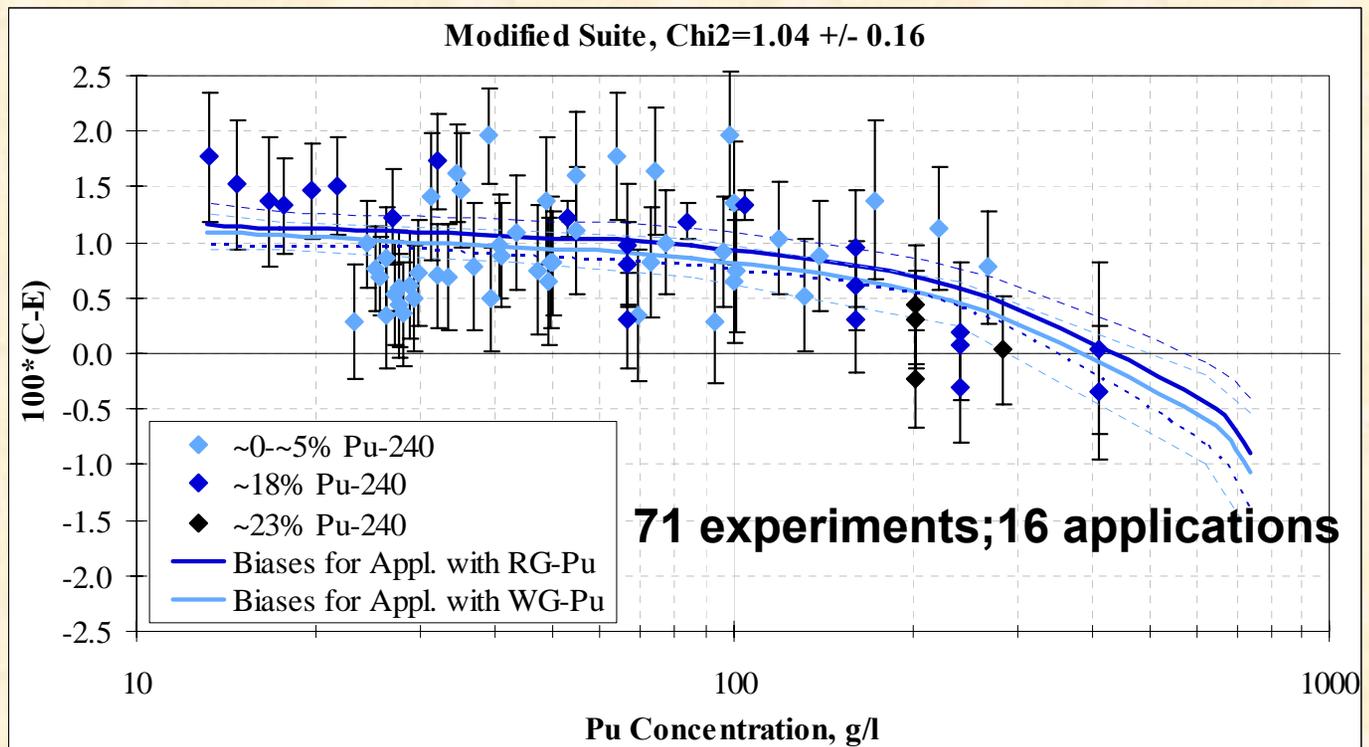
original SNL
experiments



modified experiment

Generalized Least-Squares Consolidation of Differential and Integral Data

- Computes “best” data adjustments to minimize differences in computed and measured integral experiments
- Propagates adjustments to application to estimate computational **bias** and **uncertainty**



Summary

- S/U methods can play important role in data assessment for in-reactor as well as ex-reactor components of AFC
- TSUNAMI code system provides unified set of S/U tools for ACF applications
 - Computation of sensitivities with 3D Monte Carlo or 1D discrete ordinates transport theory
 - Determination of implicit sensitivity due to self-shielding
 - Availability of approximate, extended covariance library
 - Computation of uncertainties for in-core and ex-core responses
 - Similarity analysis between proposed facility designs and integral experiments for validation
 - Consolidation of integral /differential data for improved estimates of facility design parameters